

Deposition of multicomponent coatings by Cold Spray

Ecole Nationale d'Ingénieurs de Saint-Etienne (ENISE), DIPI Laboratory,
58 rue Jean Parot, 42023 Saint -Etienne Cedex 2, France
Contact person: Prof. Igor SMUROV
e-mail : smurov@enise.fr;



Objectives

The objectives of the present study is to up-grade the cold spray technology for spraying of multicomponent coatings with the mixture preparation directly in the gas flow.

To reach this goal a new design of the cold spray nozzle was developed and the following advancements were achieved:

- Calculation of the gas parameters in the nozzle for the case of subsonic and supersonic flows mixing.
- Calculation of the particles outlet parameters (velocity and temperature values) depending on the location of the powder injection point.
- Experimental testing of the nozzle with spraying of different multicomponent coatings.

Main equations

Equations for calculation of particles velocity and temperature

$$m_p v_p \frac{dv_p}{dz} + C_p \rho_p (v - v_p)^2 = S_{solid}$$

$$\rho_p v_p c_p \frac{dT_p}{dz} = Nu \frac{6\lambda}{d_p^2} (T_0 - T_p)$$

Approximation of Henderson

$$M_p = \frac{v - v_p}{c} \frac{\rho_p (v - v_p)^2}{\mu}$$

$$Re_p = \frac{(v - v_p) d_p \rho_p}{\mu}$$

$$C_{11} = \frac{24}{Re_p + 3.06\sqrt{\gamma}} + \frac{4.5 + 0.0114 Re_p + 0.182\sqrt{Re_p}}{1 + 0.03 Re_p + 0.48\sqrt{Re_p}} + 0.3$$

$$C_{12} = C_{11} + 0.1 M_p^2 + 0.2 M_p^3 - 0.3$$

$$C_x = \begin{cases} C_{11}, & M_p < 1 \\ C_{12}, & M_p > 1.75 \\ C_{11} + 1.3(M_p - 1) \left(0.9 + \frac{0.34}{1.75} C_{11} \right), & 1 < M_p < 1.75 \end{cases}$$

Equations for calculation of gas parameters

$$\sqrt{(n+1)(n+n\theta+\theta)z(\lambda_s)} = z(\lambda_s) + n\sqrt{\theta}z(\lambda_s)$$

$$z(\lambda) = \lambda + \frac{1}{\lambda}; \theta = \frac{T_2}{T_1}; n = \frac{q(\lambda_s)}{\Pi \alpha \sqrt{\theta} q(\lambda)}$$

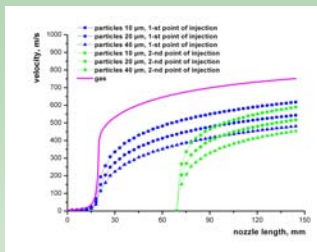
$$\Pi = \frac{P_{01}}{P_{02}}; q(\lambda) = 1.58 \lambda (1 - 0.167 \lambda^2)^{2.5}$$

$$\frac{P_{01}}{P_{02}} = \frac{\sqrt{(n+1)(1+n\theta+\theta)q(\lambda_s)}}{1 + \frac{1}{\alpha} q(\lambda)}$$

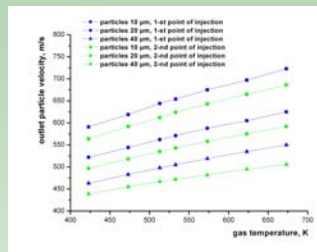
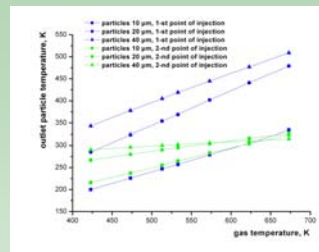
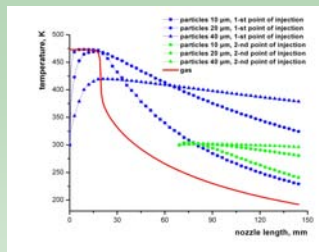
$$\frac{dM}{M} = \frac{\left(1 + \frac{k-1}{2} M^2\right) \left(\frac{dS}{S} - \frac{kF dx}{\rho a^2 S}\right)}{M^2 - 1}$$

Equations to calculate gas and particle parameters

Calculation of gas and particle parameters



$V_1 = V_2$
 $T_1 > T_2$



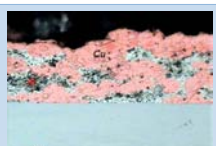
Evolution of the particle velocity in the nozzle.

Evolution of the particle temperature in the nozzle.

Calculation of the particle outlet temperature

Calculation of the particle outlet velocity

Examples of the sprayed multicomponent coatings



Cu+Al coating on aluminium substrate
Initial composition of the mixture:
50%Cu - 50%Al



Ti+Cu coating on steel substrate
Initial composition of the mixture:
50%Cu - 50%Ti

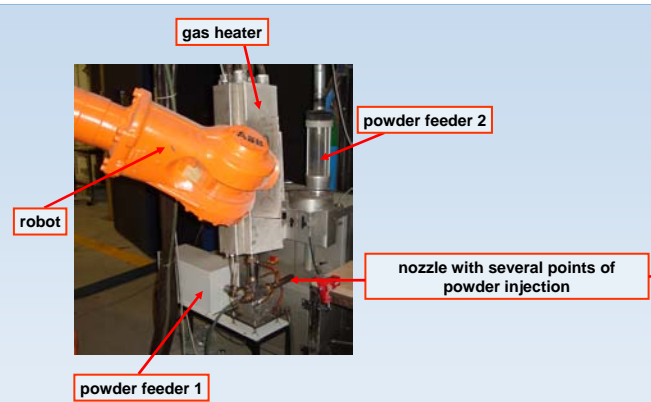


Ti+Al coating on steel substrate
Initial composition of the mixture:
30%Al - 70%Ti



Cu+Al+SiC coating on steel substrate
Initial composition of the mixture:
30%Cu - 40%Al - 30%SiC

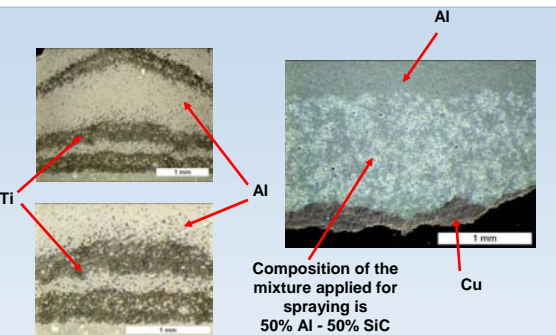
Experimental setup



Main parameters	
Gas pressure	10 – 30 MPa
Gas temperature	up to 600 °C
Gas consumption	0,5 – 2 m ³ /s
Electric consumption	1 – 30 kW

- Advantages:**
- It is possible to vary concentration of each powder component during spraying
 - Particles of each component have the optimal value of velocity and temperature

Spraying of graded coatings



Graded coatings were sprayed on Al substrate.

Conclusions

A new design of the cold spray nozzle with two points of powder injection is proposed.
Several multicomponent coatings including graded ones were successfully sprayed.